# Risk Assessment of Gas Condensates Export Pipelines by Indexing Method (Case Study: Special Economic Energy Zone of South Pars-Assaluyeh)

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Received: January 1, 2017	Accepted: January 15, 2017	Online Published: May 31, 2017
doi:10.5539/jsd.v10n3p175	URL: https://doi.o	org/10.5539/jsd.v10n3p175

#### Abstract

Due to the sensitivity and vital and undeniable role of gas energy in the energy basket of the country, especially in economy, evaluation of risk assessment studies on the designing and exploiting of this massive and extensive industry including oil and gas pipelines seems to be very necessary. Generally, risk assessment is process of the determining the risk quantity and quality by analyzing potential risks in the project which will be done by taking into account the sensitivity or vulnerability of the surrounding environment. kent Muhlbauer's method based on relative scoring of parameters that are involved in risks creation deals with the risk assessment. In order to establishment this system for risk assessment of statistical data collection, due to the failure of Iranian oil and gas pipelines, experts and scholars' experiences as a field project (South Pars gas condensate export pipeline) were collected. According to the existing conditions and availability of information sources in the Iranian oil and gas industry, finally, these data as safety risk assessment criteria of pipelines were processed in a graph and scoring was conducted based on the relative weighting of risk starter elements in the pipeline. according to the obtained scores and the relative risk of different areas of pipeline by considering km scale of areas, it was identified that 16% of the total pipeline had very high risk level, 34% of the total pipeline had medium risk level and 16% of the pipeline had low risk level

Keywords: risk, pipeline, gas condensate, indexing, Kent Muhlbauer

#### 1. Introduction

### 1.1 Introduce the Problem

Oil and gas from the first days of the eruption, always have been the driving force of the society towards progress and development and Iran with more than 30,000 kilometers of oil and gas transmission pipelines, is one of the leading countries in the operation and exploitation of this huge and valuable infrastructure. Oil and gas pipelines have been considered as the main pillars of the transfer process and according to the expansion of these lines in different facility or even residential regions and high potential of vulnerability, pipeline safety is of utmost importance [8]. Environmental risk assessment is a potential qualitative and quantitative risk analysis process and by considering sensitivity or vulnerability of its surrounding environment, it is the prediction process of potential risk [12]. Iranian Oil Terminals Company, with respect to the development of oil and gas fields and 20-year vision of development of the oil industry and the subsequent development of gas condensates export, since 2003 is located in the South Pars region and now export, totally, 600 thousand gas condensates barrels per day through pipelines and the floating buoy which are produced by South Pars refineries. So traversing a relatively long way from production to export requires a safety management system and detailed assessment at any time and any negligence and error will cause financial losses, losses in lives and damage to the environment [Map1, 2 and Figure 1]. Nowadays, safety knowledge as an integral part of human life has always been used in reducing adverse events and incidents, especially in the industrial sector of each country [14]. Now in all over the world, the pipeline risk assessment is done by methods such as FMEA / FTA/HAZOP that each has its own advantages but the new appraisal method that is designed by Kent Muhlbauer is devoted to pipelines risk assessment and now in our country, the need of using this method for planning and managing is felt and some processes have been done on the natural gas transmission pipelines [2, 5, 6]. In this study, it is intended that after a thorough acquaintance with operational processes of the transfer and Gas Condensates export, to take into account the examining and evaluating process of the pipelines risks of by indexing method; that its result leads to approaches for reducing or eliminating risks of the current activities, decreasing faults and reducing the environmental impact of gas pipelines and the promoting installations safety and the continuing the export process [1]. Therefore this research seems to be necessary. Goudarzi et al (2012), conduct a study entitled "Pipeline risk assessment by using indigenous Kenneth Muhlbauer methods, case study: Qazvin-Delijan gas pipeline" that according to the obtained results with this method, it was concluded that 32% of the pipeline had very high risk level, 11% of the total pipeline had high risk level, 23% of the pipeline had medium risk level and 34% of the total had low risk level [3].



Map 1. Satellite map of the location of case study



Map 2. Satellite map of the pipeline route of case study

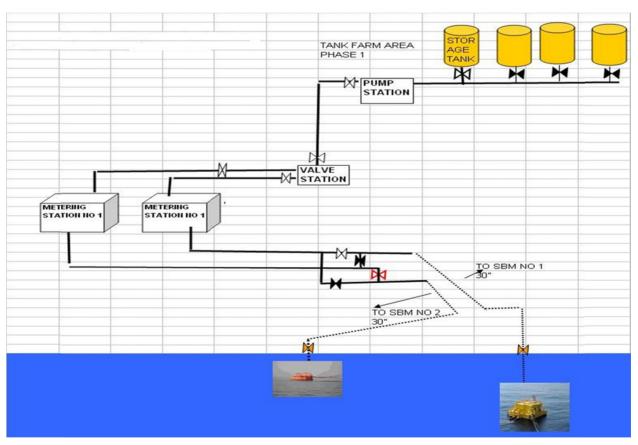


Figure 1. The pipeline route diagram of case study

### 2. Method

In this research, for collecting data, library method and analyzing documentation of under study area gas pipeline and comparing data recorded in the comprehensive maintenance system that it was used as software in the company were done and based on indexing method (on the basis of W. Kent Muhlbauer Method) in an identified assessment system and finally, with regard to range of scores and history studied by experts and administrative connoisseurs, risk assessment was carried out. [4, 9] The population of this study, in terms of questionnaire respondents, was National Iranian Oil Company experts in engineering, implementation and maintenance and statistical sample of officials as respondents in the study are relevant to these pipelines. Statistical population of this study in terms of pipelines was Assaluyeh export pipelines and in terms of samples selection for pipelines risk assessment was gas condensates exporting pipeline which are produced at gas refineries located in South Pars [Figure 2]. Indexing method(on the basis of W. Kent Muhlbauer Method) calculated pipelines risks and the possible threats in pipeline which are third party damage pipelines risks, corrosion, design and incorrect operation were calculated by a relative scoring system. [10] In other words, first the main risk factors were defined and Algebraically summed in each stage and the total risks index for different parts of the pipeline were obtained and health and environmental risk factors for these periods were calculated and multiplied together and we determine the severity of leakage impact index [11] and finally levels of safety risk factors of each section were divided based on health and environmental risk factors that the resulting number shows relative risk of any section of pipeline and easily by observing the risk level of pipeline section, the critical points can be determined and we can plan to reduce critical points and eventually using tables and graphs the final analysis is done. [13]

The associated formulas are:

**Total Risk (Sum Index)** =Third party damage Index+ Corrosion Index+ Design Index+ Incorrect operation Index

Leak impact factors index = Product hazard\* leak volume \* Dispersion\* Receptors

**Relative risk Score** = Total Risk Index divided by the Leakage impact factors index

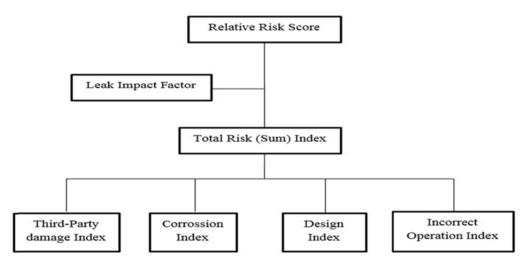


Figure 2. Risk assessment model by indexing method

The first step in the risk assessment of gas condensates export pipelines is division of pipeline to obtain the risk number. In this study the pipelines dividing was done based on dynamic approach and the under study pipeline has been divided into 6 sections **[Table 1]** that was used as the most appropriate method for division of lines and based on criteria such as population density surrounding the pipeline, pipe thickness, pipe diameter **[Table 2]** and the equipment on the ground, markers, the area surrounding the pipeline (with regard to construction, type of land use change) and natural features this division was done.

Table 1. Pipelines division of case study

Pipeline length	Section 1	Section2	Section3	Section4	Section5	Section6
11933 m	150 m	2000 m	1700 m	1631 m	3800 m	2652 m

Diamete	Thickness r	Coverage type	Pressure	pressure	temperature
Carbon-Steel Pipeline 30 Inche API =5LX52	s 15.9 mm	Three-layer polyethylene	Psi 300	90 Psi	20-45°C

#### Table 2. Pipeline characteristics of case study

#### 3. Results

In this study, according to the conducted studies, dynamic method has been used in the pipeline division. Since the under study area contained Manifold valves stations and installations for the measurement of gas condensates export pipelines from refineries, during the 11-kilometer of the pipeline, manifold taps, climate change, pipeline circumstances and pipeline route change were used as dividing point. In **[Table 3]** the third-party damage index variables and points are shown.

Table 3. Assessment of third-	party damage index variables

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section 6		
	Depth of cover							
Score	20	20	20	20	20	20		
Description / Calculations	Surface of the ground	Underground	Underground	Underwater	Underground	Underwater		
			Activity Leve	el				
Score	8	8	8	15	8	15		
Description / Calculations		Medium		Low	Medium	Low		
		A	Aboveground Fac	ilities				
Score	10	7	0	10	7	10		
Description / Calculations	Pipelines junction / co	onveyor construct	ion and Pardis po	etrochemical Ca	mpus / pipeline	passageway		
		Iden	tification of risk	location				
Score	15	15	15	15	15	15		
Description / Calculations	Case study in sit	te one and under	the supervision o	f South Pars Sp	ecial Economic	Zone		
			Public educati	on				
Score	15	15	15	15	15	15		
Description / Calculations	Joint m	eetings between t	he oil and gas co	mpanies and lo	cal authorities			
		R	ight-of- way con	ditions				
Score	5	2	2	3	4	3		
Description / Calculations	Great	Medium	Medium	Good	Good	Good		
		Patro	l Frequency and	inspection				
Score	15	15	12	12	15	12		
Description / Calculations			Limit	ation		Limitation		
Third party damage index	88	82	72	90	84	90		

In [Table 4] corrosion index variables and Scores are shown:

#### Table 4. Assessment of corrosion index variable

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section
		A	mospheric Expo	osures		
Score	4	4	5	5	4	5
Description / Calculations	Soil - air interface	;			Soil - air interface	
			Atmospheric Ty	pe		
Score	1.2	0.5	0.8	0.8	0.8	0.8
Description / Calculations	Extreme humidity and high temperature	Ch	emical and extre	eme humidity / ma	arine and wetland-co	oastal
		I	Atmospheric Coa	ting		
Score	5	3	3	3	3	3
Description / Calculations						
			Product Corrosiv	vity		
Score	7	7	7	7	7	7
Description / Calculations	Gas condensates cor	rosion is not inc	luding and corro	sive under certain	o conditions is possi	ble
		(	Corrosion prever	tion		
Score	10	3	3	3	3	3
Description / Calculations	Observations	Pigging, inter	nal laminated an	d inhibiting subst	ances injections hav	en't taken pla
			Soil corrosivit	у		
Score	15	9.25	9.25	7	9.25	7
Description / Calculations	1000 - 15,000 ohm-cm soil resista induced corrosion (MIC) was not		on average, pH=	4-8 suitable, hum	idity 20-30% and m	nicrobially
			Iechanical Corro	osion		
Score	3		1echanical Corro	osion 3	3	3
Score Description / Calculations	3 Operating pressure of less than 60 10 years old pipeline and three-la	N 3 0% of the submis	3 ssion (Design pr	3 essure), operating		
	Operating pressure of less than 60	3 0% of the submis yer polyethylene	3 ssion (Design pr	3 essure), operating of pipes		
	Operating pressure of less than 60	3 0% of the submis yer polyethylene	3 ssion (Design pro- coating system	3 essure), operating of pipes		
Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la	N 3 0% of the submis yer polyethylene 0.15	3 sision (Design pro- coating system Cathodic protect 0.15	3 essure), operating of pipes ion 1.5	temperature less th	an 38 °C, ab
Description / Calculations Score	Operating pressure of less than 60 10 years old pipeline and three-la 15	N 3 0% of the submis yer polyethylene 0.15 No cathe	3 sision (Design pro- coating system Cathodic protect 0.15	3 essure), operating of pipes tion 1.5 ystem / The distar	temperature less th	an 38 °C, abo
Description / Calculations Score	Operating pressure of less than 60 10 years old pipeline and three-la 15	N 3 0% of the submis yer polyethylene 0.15 No cathe	3 ssion (Design pro- e coating system Cathodic protect 0.15 odic protection s	3 essure), operating of pipes tion 1.5 ystem / The distar	temperature less th	an 38 °C, ab
Description / Calculations Score Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System	N 3 0% of the submis yer polyethylene 0.15 No catho A(	3 sision (Design pro- e coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absent	3 essure), operating of pipes ion 1.5 ystem / The distar rences	1.5 nce between test poi	an 38 °C, abo 1.5 int <1.5 km 3
Description / Calculations Score Description / Calculations Score	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2	N 3 0% of the submis yer polyethylene 0.15 No catho 2	3 sision (Design pro- e coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absent	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 te of power sion lines	1.5 nce between test point	an 38 °C, abo 1.5 int <1.5 km
Description / Calculations Score Description / Calculations Score	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2	N 3 0% of the submis yer polyethylene 0.15 No catho 2	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absence transmis	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 te of power sion lines	1.5 nce between test point	an 38 °C, abo 1.5 int <1.5 km 3
Description / Calculations Score Description / Calculations Score Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1	N 3 0% of the submis yer polyethylene 0.15 No cather 2 20Kv 1	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absend transmiss Impact of guar 1	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ee of power sion lines ds	temperature less th 1.5 nce between test poi 2 20Kv 1	an 38 °C, abd 1.5 int <1.5 km 3 None
Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations Score	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1	N 3 0% of the submis yer polyethylene 0.15 No cathe 2 20Kv 1 crossing point an	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absend transmiss Impact of guar 1	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ce of power sion lines ds 1 e are necessary co	temperature less th 1.5 nce between test poi 2 20Kv 1	an 38 °C, abd 1.5 int <1.5 km 3 None
Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations Score	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1	N 3 0% of the submis yer polyethylene 0.15 No cathe 2 20Kv 1 crossing point an	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absence transmiss Impact of guar 1 d underpass ther	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ce of power sion lines ds 1 e are necessary co	temperature less th 1.5 nce between test poi 2 20Kv 1	an 38 °C, abo 1.5 int <1.5 km 3 None
Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1 1 At the c	N 3 0% of the submis yer polyethylene 0.15 No catho 2 20Kv 1 crossing point an D 5.5	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absence transmiss Impact of guar 1 d underpass ther C current interfer 1.5	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ce of power sion lines ds 1 e are necessary co rence 7	temperature less th 1.5 nce between test poi 2 20Kv 1 ontrivance	an 38 °C, abd 1.5 int <1.5 km 3 None 1 7
Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1 1 At the c 7	N 3 0% of the submis yer polyethylene 0.15 No catho 2 20Kv 1 crossing point an D 5.5	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absence transmiss Impact of guar 1 d underpass ther C current interfer 1.5	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ce of power sion lines ds 1 e are necessary co rence 7 d parallel to gas of	temperature less th 1.5 nce between test poi 2 20Kv 1 ontrivance 6.5	an 38 °C, abd 1.5 int <1.5 km 3 None 1 7
Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations Score Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1 1 At the c 7	N 3 0% of the submis yer polyethylene 0.15 No catho 2 20Kv 1 crossing point an D 5.5	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absend transmiss Impact of guar 1 d underpass ther C current interfer 1.5 pipeline cross ar	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ce of power sion lines ds 1 e are necessary co rence 7 d parallel to gas of	temperature less th 1.5 nce between test poi 2 20Kv 1 ontrivance 6.5	an 38 °C, abd 1.5 int <1.5 km 3 None 1 7
Description / Calculations Score Description / Calculations	Operating pressure of less than 60 10 years old pipeline and three-la 15 cathodic protection System 2 63Kv 1 1 At the c 7 None	N 3 0% of the submis yer polyethylene 0.15 No catho 2 20Kv 1 crossing point an D 5.5 There are 20 25	3 sision (Design pro- coating system Cathodic protect 0.15 odic protection s C current interfer 3 The absence transmiss Impact of guar 1 d underpass ther C current interfer 1.5 pipeline cross ar Pipe covering	3 essure), operating of pipes ion 1.5 ystem / The distar rences 3 ce of power sion lines ds 1 e are necessary cor rence 7 d parallel to gas of 3 25	1.5         1.5         nce between test point         2         20Kv         1         ontrivance         6.5         condensate pipeline	an 38 °C, abd 1.5 int <1.5 km 3 None 1 7

Design Index variables and scores are shown in [Table 5]:

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section 6
			Pipe safe	ty factor		
Specifications		Flange, V	Valve, Pipeline Cla	ass300, Thickness	:15.9 mm	
Score	35	35	35	35	35	35
Description / Calculations	6	times operating a	nd utilization press	sure (90psi) and de	esign pressure 300	psi
			Fatigue	stresses		
Score	9	9	9	9	9	9
Description / Calculations		stress cycles 10	000- 10000 since th	ne establishment o	f, MAOP = 30%	
			surge p	otential		
Score	5	5	5	5	5	5
Description / Calculations	Depending on the	ne type of fluid ,lo	w pressure and low	v speed in pipeline	the possible surge	e potential is lo
			Integrity ve	erifications		
Score	15	15	15	15	15	15
Description / Calculations		Hydrostatic tes	st of pipes has not	been done for mor	e than 10 years	
			Land mo	ovements		
Score	15	5	10	10	10	10
Description / Calculations	None	Medium		Lo	ow	
Fotal corrosion index (0-100)	79	69	74	74	74	74

#### Table 5. Assessment of corrosion index variable

In [Table 6] incorrect operations index variables and scores are shown:

## Table 6. Assessment of corrosion index variable

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section 6						
Design		Hazard identification										
Score	3	3	3	3	3	3						
Description / Calculations		HAZID & H	AZOP studies are	performed at the ti	me of design							
Possibility of M.O.P			Maximum de	esign pressure								
Score	5	5	5	5	5	5						
Description / Calculations	Unlikely (applic	ation error, Installa		becific status and a numan error)	ccidental obstruction	on of middle wa						
			Safety	systems								
Score	5	5	5	5	5	5						
Description / Calculations	Level 1 safety sy	/stems / remote vie	w system / control	of some control va	alves							
			Material	selection								
Score	2	2	2	2	2	2						
Description / Calculations	Evaluatio	on and inspection o	f the product pipel	ine has been done	by the national oil	company.						
			Checks (inspect	tion and control)								
Score	2	2	2	2	2	2						
Description / Calculations	Ra	tification and Sign	ature of the constru	uction and executiv	e plans are approv	red.						
Construction			Inspection in 1	Manufacturing								
Score	10	10	10	10	10	10						
Description / Calculations	Company	supervising engine	ers adequately mo	nitor the correct in	plementation of th	ne pipeline.						
			Mate	erials								

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Score	2	2	2	2	2		2
Description / Calculations	According to the	e existing documents	s they were appr	oved by super-	vision enginee	ers.	
			Joining(Weld	ling and fitting	s)		
Score	2	2	2	2	2		2
Description / Calculations	Inspec	tion of froth and rad	iological examin	ation was con	ducted by sup	ervising er	ngineers
			Ba	ckfill			
Score	2	1	2	2	2		2
Description / Calculations		Seasonal hea	vy rainfall, pick	ing up the side	walls of pipe	eline	
			Transport	and maintain			
Score	2	2	2	2	2		2
Description / Calculations	Pip	eline transportation a	and maintenance	has been asse	ssed within ac	ceptable l	imits
			Ins	ulation		-	
Score	2	2	2	2	2		2
Description / Calculations	Froth insulation	on and padding unde	rneath the pipe e	embankment a	nd channel tu	ne up is wi	thin acceptabl
I. I				mits		<b>I</b>	
Operation		Gu	idelines and Sta	ndards and pro	cedures		
Score	5	5	5	5	5		5
Description / Calculations							
	SCADA (Sur	ervisory control and	data acquisition	) / Communic	ation		
Score	1	1	1	1	1		1
Description / Calculations	In the pipeline	e system the SCADA	system is not c	omplete, yet 8	0% Of system	is control	led by operato
•			testing				
Score	1	1	1	1		1	1
Description / Calculations	Exce	pt from the recruitm	ent time there is	no other evide	ence of person	nel drug te	esting.
	`	Safety 1	orograms				
Score	1	1		1	1	1	1
Description / Calculations	Safety pro	gram is designed bu	t it is not with a	high level of p	articipation o	f workers of	cooperation
1			haps, archive	0 1	1		1
Score	5	3	3		3	3	3
Description / Calculations	Surface fa	acilities are under the	e control but und	erground facil	ities control r	eview are	incomplete
r. r.			ining				r r
Score	6	6	0	5	6	6	6
Description / Calculations		ic understanding of the				-	-
Description / Culculations	i ensember s ousi	e understanding of t		related test.	controly sur	ierenii, out	personner are
		Mechanical e	rror preventers				
Score	5	5		5	5	5	5
Description / Calculations		There is	no Block Valve	along the way	of pipelines		
*			e and repairs		• •		
Score	15	13	13	13	13		13
Description / Calculations		nentation and approp				hev are co	
carearanting		and approp			r	-,	
•			]	IPS			
Total incorrect operations	76	71	72	IPS 72	72		72

In [Table 7] leak Impact Factor Index variables and the related scores are shown.

### Table 7. Assessment of corrosion index variable

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section 6	
	I	Flammability(N1	)				
Score	3	3	3	3	3	3	
Description / Calculations		,	The flash point i	s less than 100°l	F		
		Reactivity(Nr)					
Score	0	0	0	0	0	0	
Description / Calculations	5	Stable materials	that even when	heating stay stab	le and unreactiv	e	
			toxici	ty(Nh)			
Score	2	2	2	2	2	2	
Description / Calculations		Μ	edical care is ne	eded when expo	sed		
			chronic ha	azard (RQ)			
Score	2	2	2	2	2	2	
Description / Calculations	Surface, underground and underwater Pipelines, RQ=5000						
	LC50=5000ppm,LD50=3160mg/kg skin						
			leak v	volume			
Score	1	1	1	1	1	1	
Description / Calculations			pipeline mater	ial=API 5LX52			
		Dispersion					
Score	1	1	1	1	1	1	
Description / Calculations			Soil type (sa	andy, gravel)			
Receptors and the environment and High			R=POP + E	ENV + HVA			
valuable areas							
Score	5.1	5.7	6.2 5	.2	5.7	5.2	
Description / Calculations	P>46, DOT	(Department Of	Transportation)	TYPE 3=5 SCC	ORE Adjacent in	dustries, the	
			industri	al estate			
			LIF=PH*	*LV*D*R			
leak Impact Factors Index	35.7	39.9	43.4	36.4	39.9	36.4	

Finally in [Tables 8, 9] sum and averages index and in [Tables 10, 11] relative risk score and overall risk assessment are shown:

Table 8	Sum	indexes	(total	risk)
10010 0	~~~~			

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section 6
Total third-party damage index	88	82	72	90	84	90
Total corrosion index	95.2	63.4	61.4	66.3	66.05	66.3
Total design index	79	69	74	74	74	74
Total incorrect operations Index	76	71	72	72	72	72
Sum indexes (0-400)	338.2	285.4	281.4	302.3	296.05	302.3

Index	Third-party damage index	Corrosion index	Design index	incorrect operations Index
Section 1	88	95.2	79	76
Section 2	82	63.4	69	71
Section 3	72	61.4	74	72
Section 4	90	66.3	74	72
Section 5	84	66.05	74	72
Section 6	90	66.3	74	72
Average	84.3	69.77	74	72.5

#### Table 9. Average of total risk (safety) indexes

Table 10. Average of total risk (safety) indexes

Pipeline	Section 1	Section 2	Section 3	Section 4	Section 5	Section 6
Sum Indexes (SI)	338.2	285.4	281.4	302.3	296.05	302.3
leak Impact Factor Index (LIF)	35.7	39.9	43.4	36.4	39.9	36.4
Relative Risk score (SI/LIF)	9.47	7.15	6.48	8.3	7.4	8.3

#### Table 11. Risk Assessment of gas condensate export pipeline

Pipe	Risk Risk assessment		Percent (%)	
section	score			
Section 3	6-7	Very high	16	
Section 2 and 5	7-8	High	34	
Section 4 and 6	8-9	Medium	34	
Section 1	9-10	Low	16	

The obtained results showed that the third-party potential damage index in all areas of the pipeline were in good condition except the second and third sections that the most important factors of scores decreasing were, respectively, crossing the pipe through sulfur installations and other facilities construction (NPC) on the pipeline, lack of dedicated corridor, not specifying the service road (ROW), lack of pipeline safety privacy, non-professional licensing for construction of conveyors and petrochemical facilities on the pipeline by higher authorities without risk assessment and considering the lack of pipeline privacy and fencing and physical protection of a range, that these are increasing factors of risks, so that got lower scores compared with other places that is higher risk indicator of this areas.

The results of the evaluation of corrosion index showed that in most areas of the pipeline poor scores have been obtained. In the first area because of its surface statue, inspection and protection against corrosion were properly carried out and this process showed less risk marker than other areas, and second and third evaluated zones of pipelines have raised the chance lower scores because of 14 pipelines crossover and parallel crossing and presence of annoying and wandering currents, Atmospheric conditions change and high soil moisture in the pipeline route, 10 years old under study pipelines, the absence of integrated cathodic protection systems and pipeline pigging due to different diameters and lack of information about the actual condition of pipelines in this area compared to other areas, that is evident of more risk is in these areas.

The design index results reflect that the obtained scores, although most are in the acceptable range but are not satisfactory in the range of 2 and 3 and the most important reasons of this issue are respectively, unsafe pipeline route selection and unprofessional authority licensing for the construction of other facilities around it, chance of motion and movement of the earth, picking levee wall of the pipeline route and the retrofitting rocks and cover it with just fine soil, constructing channels to collect surface water and washing slag and soil on the pipe and lack of the pipe hydrostatic testing more than 10 years. Evaluation of design index within the second area unlike the previous indexes from the third area has gained lower scores and this issue is due to the above reason that is a sign of higher risk for this area.

In the assessment of incorrect operation index, it was clarified that with regard to the integrity of the pipeline and the impact of parameters of the index for the entire route as well as its construction by reputable and experienced foreign companies (Total & Petronas), same and acceptable scores were obtained. However, since in the past years, the results of analysis showed that human errors are the cause of the events that have occurred in gas condensate export pipelines, the assessment conducted is not satisfactory. Among the main reasons for this are, respectively, level one (low level) procedural facilities safety system, lack of SCADA systems, and 80% operator regulatory system, lack of holding occupational exams related to beneficiary employees, absence of evidence showing drug test after hiring personnel, and lack of optimal worker participation in safety programs designed.

Total results of safety indicators indicate that in the second and third sections, achieved points were not satisfactory and were riskier than other areas. Although the rest of the areas according the maximum safety index score (400) that they can gain in ideal conditions, they did not have acceptable level of scores and they were in the notification area but not paying attention to them can, in not too distant future, cause unwanted events.

So after averaging the safety indicators of the studied range, it was found that the pipelines conditions with regard to the corrosion index and the index of operation and malfunctions are in the worse than the other indices situation that it is necessary to perform precautionary measures related to the aforementioned indicators variables.

The leakage impact factors index results suggest that the leakage impact with respect to the information contained in the gas condensates SDS, NFPA704 standard and DOT 192 classification in the terms of the toxicity and health, environmentally sensitive and economically valuable areas are not in the too acute area and if rating each of the pipelines move toward zero, the severity of the consequences of leakage will be less and the only reason to increase the points of the third, second and fifth areas in compare with other regions will be the crossing of the pipeline from environmentally sensitive and economically valuable areas, and in case of leakage that could have more deleterious effects. The results of the level relative risk index that represents relative risk and total assessment and by dividing the total index with the index of the health risks and environmental impact of the leakage, showed that third section of pipe had very high risk level, the second and fifth section had high risk level, fourth and sixth sections had medium risk level and the first section had low risk level, also relative percentages with regard to the total risk level obtained with respect to the results are as: 16% of the total pipeline had a very high, 34% of the pipeline had a high, 34% of the total pipeline had medium and 16% of the total pipeline had a low risk level.

#### 4. Discussion

The highest risk of plan related to gas condensate leakage and future consequences (fire, explosion, personal accident, environmental pollution...) therefore, it is necessary that in the early designing stages (feasibility) all the factors should be assessed and evaluated using appropriate methods of risk assessment of the pipeline. Moreover, all requirements and standards of implementation and risk management program of pipeline should be considered from the beginning, and in case of making corrections and modify in the pipeline and its environmental conditions, management of change program must be institutionalized and implemented in the company.

Pipelines threatening factors and variables vary from state to state and appropriate preventive measures specific to each region should be considered

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